

PIV Investigations of LSB Flames

Need to Obtain More Details of the Development of LSB Flowfields



- **Simulation of air-jet LSB in progress**
 - yet to achieve stable solution due to complexities of interaction between core flow, swirling flow and freely propagating flame
- **Previous LDV data not sufficiently extensive for direct comparison**
 - needs better characterization of outer swirling flow region, self-similarity, downstream recirculation and swirl number effects
- **Rectified swirl number definition for air-jet LSB**
 - Previous definition derived from equation for a special case
 - New definition compatible with definition for vane LSB

$$S = \frac{\pi R_e R}{A_j} \left(\frac{\dot{m}_j}{\dot{m}_{total}} \right)^2$$

R_e = burner radius **R** = injector radius

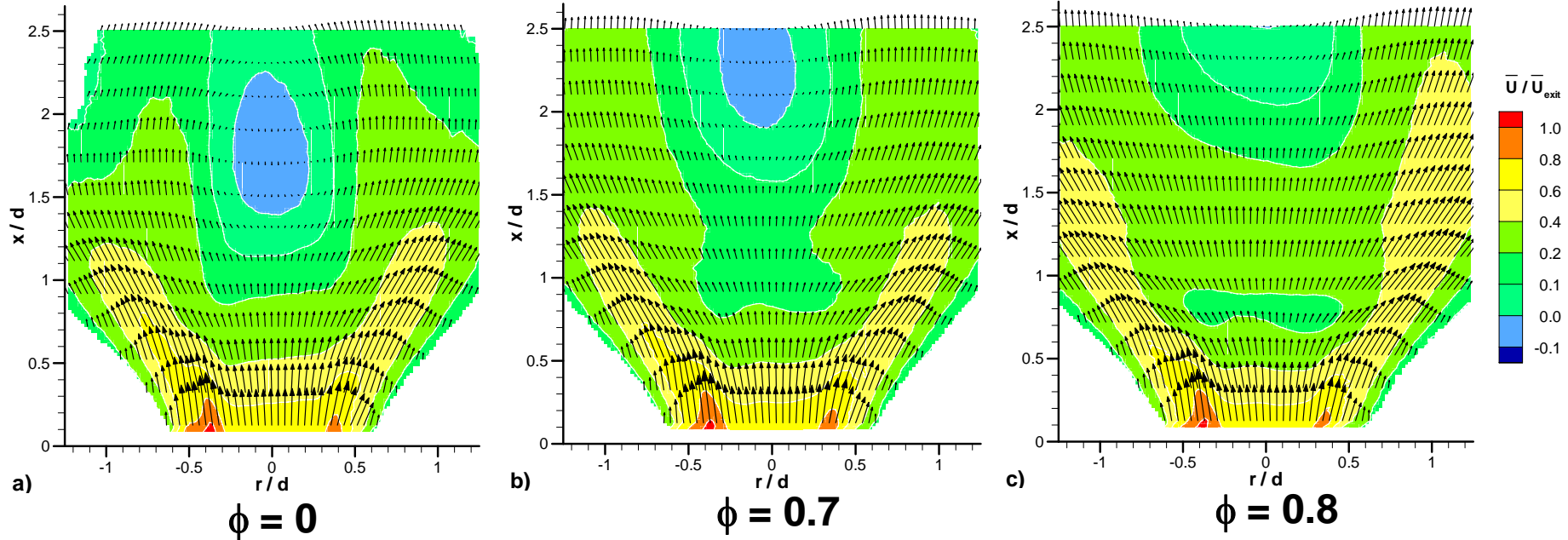
A_j = total area of the swirl jets

\dot{m}_j = total mass flow rate of swirl

\dot{m}_{total} = total mass flow rate of reactants

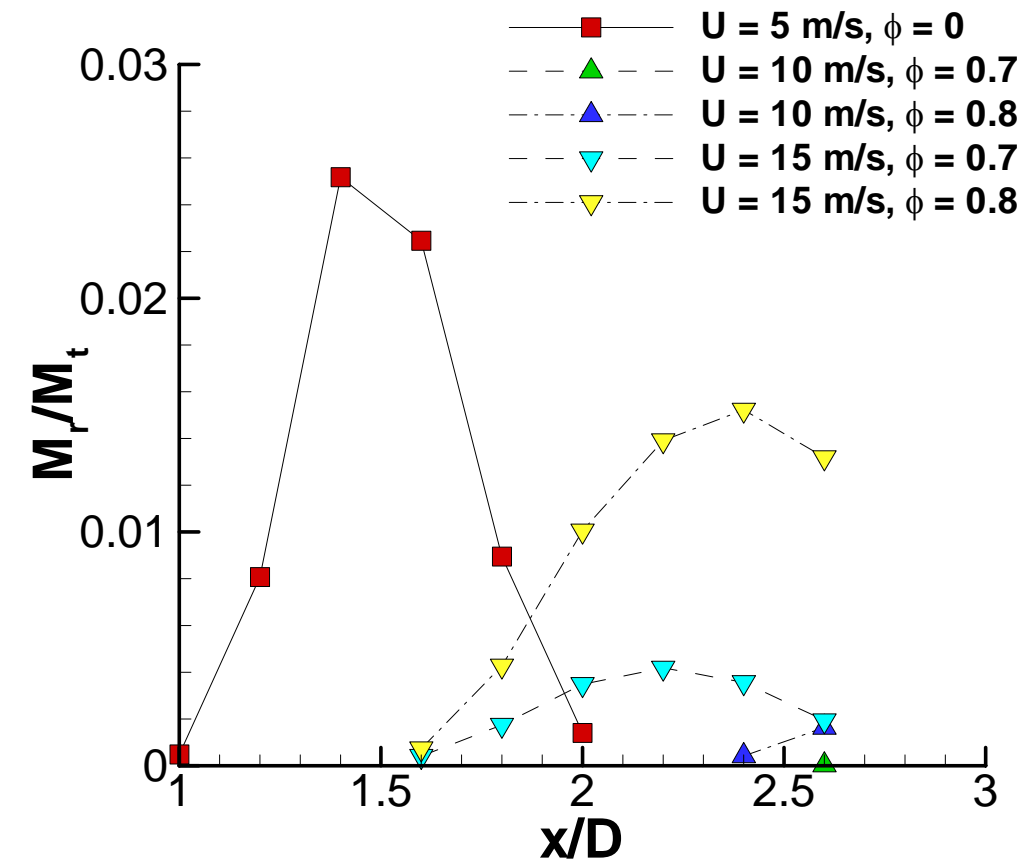
Downstream Flow Recirculation Weakened by Combustion Heat Release

$S=0.85$ and $Re \approx 37,000$ $U \approx 10.5$ m/s



- PIV with a large field of view shows the formation of a downstream recirculation bubble at $x/D > 1$
- Downstream recirculation does not affect flame brushes in the upstream region ($x/D < 1$)

Quantifying Recirculation Strength



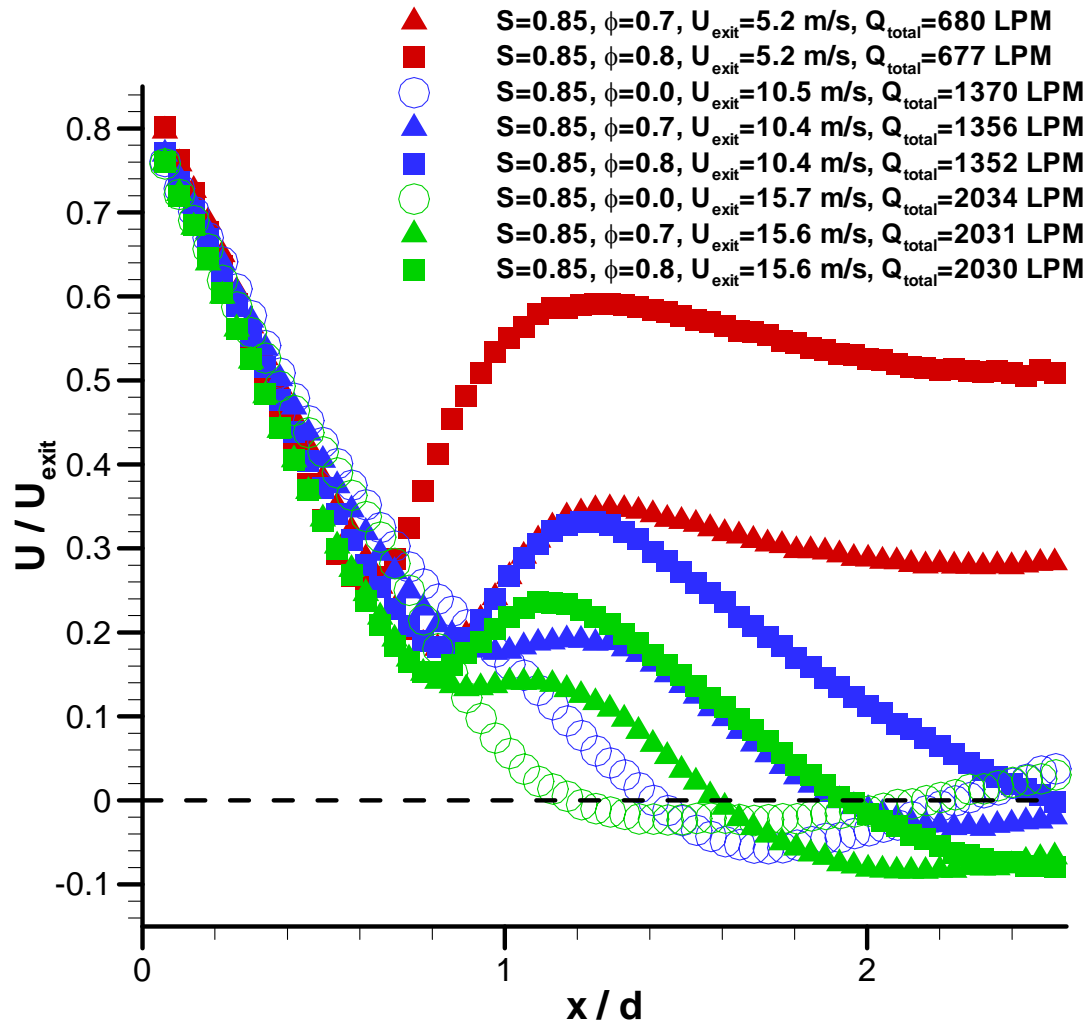
- Reversed mass flow rate

$$M_r = \int_0^{y_0} 2\pi y \rho U dy$$

y_0 = zero velocity boundary

- Recirculation strength increases non-linearly with S
- Typical values of M_r/M_t in LSB are 10 orders of magnitude lower than in typical high swirl burners (up to $M_r/M_t = 2$)
- Provides another critical test for simulation

Similarity Found In LSB Flowfield



- Normalized centerline profile shows consistent linear decay of mean axial velocity at the exit
- Explains why flame brush remains stationary with increasing U
- New and important insight on the mechanism of low-swirl flame stabilization

Studies of Thermal/Diffusive Instability in Turbulent Flames

Flame Front Instabilities in Turbulent Flames



- Wrinkling introduces flame front curvatures, as well as flame front compression or stretch
- Local flame speed on the flame fronts, s , is proportional to stretch via the relationship

$$s/s_L = 1 - Ma Ka_L$$

Ma is the Markstein number

Ka_L is the Karlovitz number for a local stretch rate

- Studies of flames with moderate turbulence show thermal/diffusive instabilities and hydrodynamic instabilities either dampen or promote flame wrinkle formation
- Quasi-steady DNS studies (Im and Chen) suggest impact of thermal/diffusive instabilities diminishing at frequencies > 200 1/sec

Investigate the Significance of Thermal/Diffusive Instability



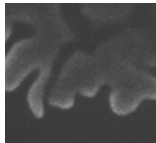
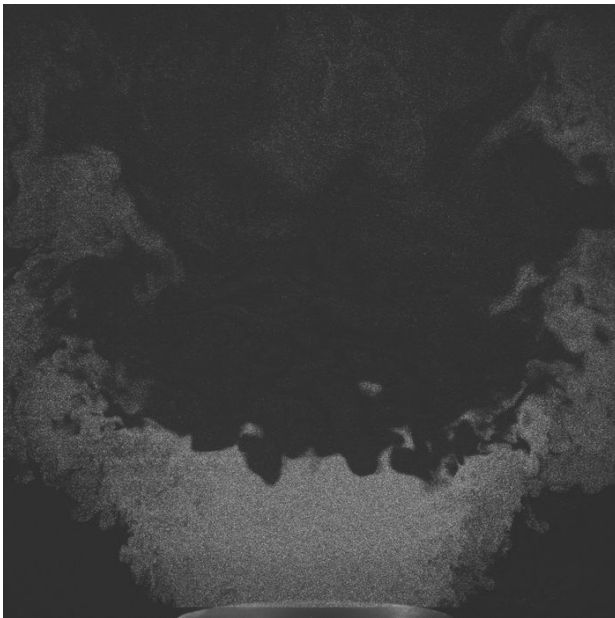
- **How chemistry affects the flowfield has yet to be addressed in complex flame configurations**
 - Previous studies involved flame interacting with a single large vortex or at relatively low turbulence
- **Exploit the unique capability of low-swirl burner to investigate systematically nine H_2 , CH_4 and C_3H_8 flames**
 - $S = 0.8$, $U_o = 5 - 15$ m/s, $\phi_{H_2} = 0.3$ $\phi_{CH_4} = 0.8$ & $\phi_{C_3H_8} = 0.75$
- **Safety concerns on burning pure H_2 limited the experimental conditions to low to moderate turbulence**
 - Still relevant based on statistical argument
 $57 < u'/l_x < 210 \text{ sec}^{-1}$ for $5 < U_o < 15$ m/s
comparable to eddy turnover frequency $s_L/d_L = 300 \text{ sec}^{-1}$

- **Experiments completed**
 - **PIV (448 image pairs)**
 - Large field of view (13 by 13 cm)
 - Conditioned velocities using oil aerosol
 - Unconditioned velocities using refractory seeds OH-PLIF (200 images)
 - Smaller field of view (3 by 3 cm)
- **Analysis**
 - Mean and rms flowfields (complete)
 - Displacement flame speed (complete)
 - Flame front curvature distributions (in progress)

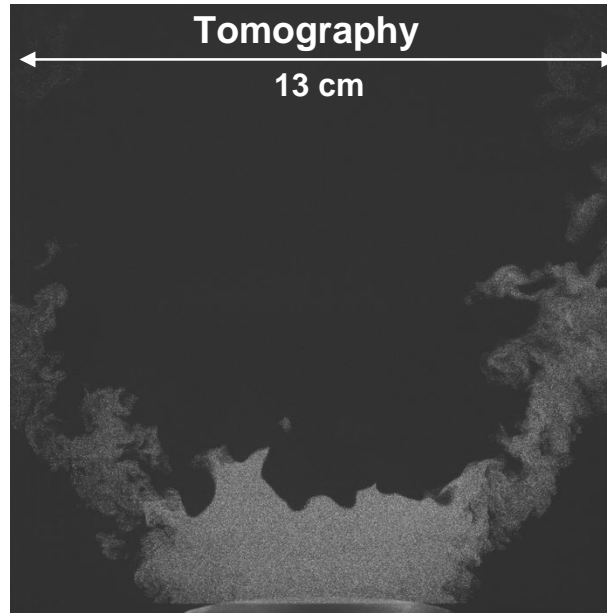
Flame Wrinkle Structures at $U_o = 5 \text{ m/s}$, $u'/l_x = 57 \text{ sec}^{-1}$



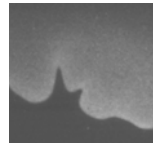
H_2 , $\phi = 0.3$, $\text{Le} = 0.33$



CH_4 , $\phi = 0.8$, $\text{Le} \approx 1$

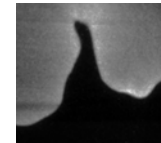
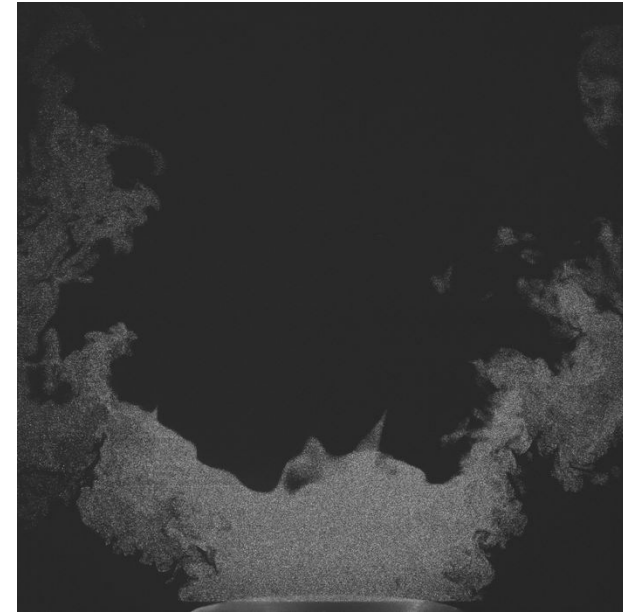


OH-PLIF



3 cm

C_3H_8 , $\phi = 0.75$, $\text{Le} = 1.85$

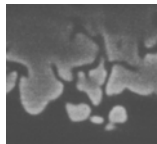
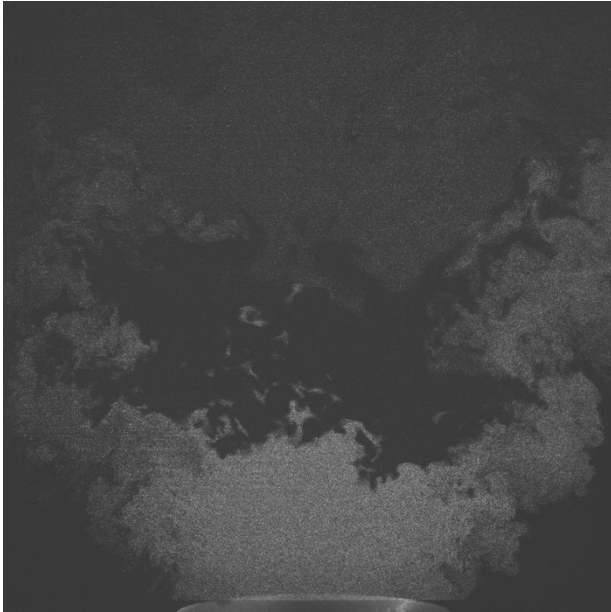


- Difference in flame wrinkle structures readily observable

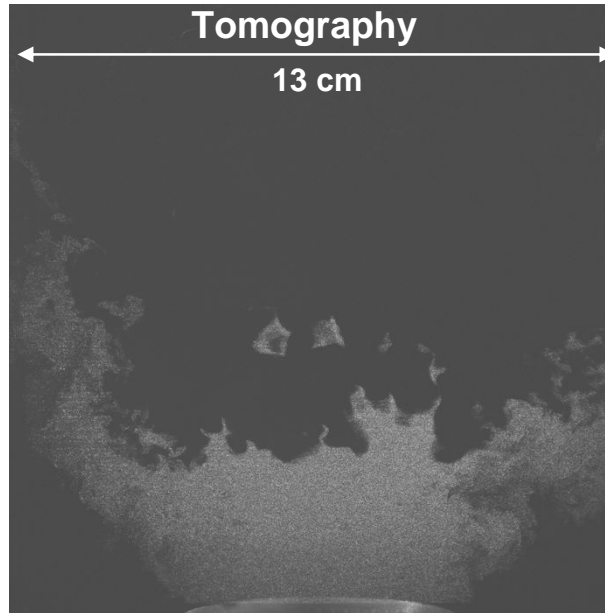
Flame Wrinkle Structures at $U_o = 15 \text{ m/s}$, $u'/l_x = 210 \text{ sec}^{-1}$



H_2 , $\phi = 0.3$, $\text{Le} = 0.33$



CH_4 , $\phi = 0.8$, $\text{Le} \approx 1$



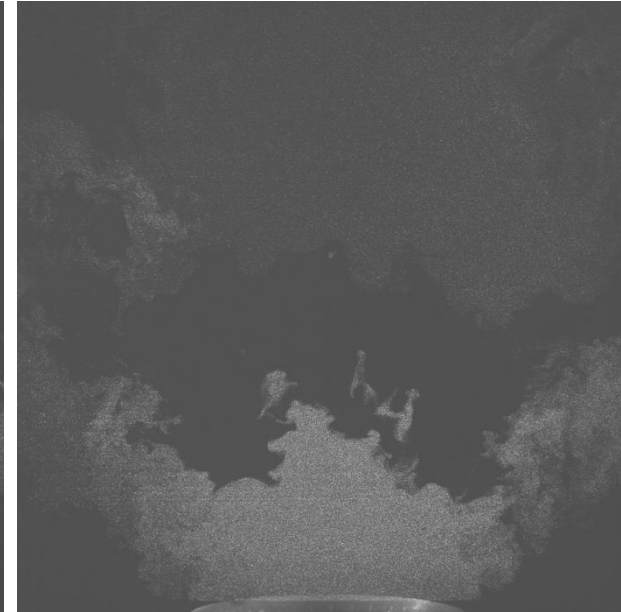
OH-PLIF



3 cm

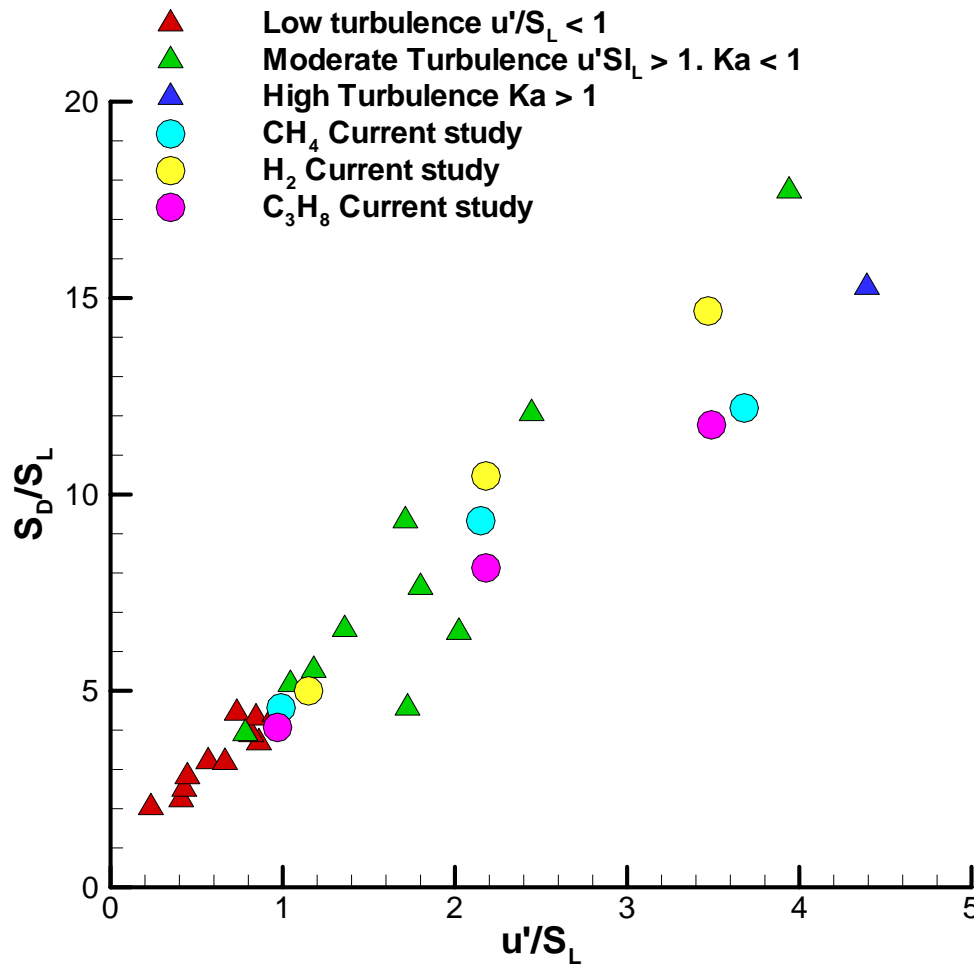


C_3H_8 , $\phi = 0.75$, $\text{Le} = 1.85$



- Differences in flame wrinkle structures persist

Small Differences Found in Displacement Flame Speeds, S_D , of H_2 , CH_4 and C_3H_8 Flames



- PIV data obtained using oil aerosol determine flame brush positions, S_D , and u'
- S_D for all nine flames consistent with those obtained previously for CH_4
- Differences in flame zone divergence implies possible effects on S_c